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## A SVAT Scheme for NO, NO<sub>2</sub>, and O<sub>3</sub> – Model Description and Test Results

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With 9 Figures

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### Summary

A soil/vegetation/atmosphere transfer (SVAT) scheme for determining the dry deposition and/or emission fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> in the atmospheric surface layer over horizontally uniform terrain covered with fibrous canopy elements is presented and discussed. This transfer scheme is based on the micrometeorological ideas of the transfer of momentum, heat and matter near the Earth's surface, where chemical reactions between these trace gases are included. The fluxes are parameterized by first-order closure principles. The uptake processes by vegetation and soil are described in accord with Deardorff (1978). The SVAT scheme requires only routine data of wind speed, dry- and wet-bulb temperatures, short wave and long wave radiation, and the concentrations of O<sub>3</sub> and nitrogen species provided by stations of monitoring networks.

First model results indicate that the dry deposition fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> are not only influenced by meteorological and plant-physiological parameters, but also by chemical reactions between these trace species and by NO emission from the soil. Furthermore, a small displacement in the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> within in the range of the detection limits of the chemical sensors can produce large discrepancies in the flux estimates, which are manifested here by the shift from height-invariant fluxes substantiated by the photostationary state to strongly height-dependent fluxes caused by the departure from that state. Especially in the case of these nitrogen species the widely used 'big leaf' multiple resistance approach, which is based on

the constant flux approximation seems to be inappropriate for computing dry deposition fluxes and deposition velocities.

### 1. Introduction

It is well established that dry deposition plays an important role in the mass budget of many gaseous species (Businger, 1986). This removal process generally depends on the micrometeorological transfer properties of the atmospheric surface layer, the capability of vegetation and soil to take up matter, and the prevailing chemical and photochemical environment. It can directly be determined by eddy correlation techniques and/or by enclosure techniques (static and dynamic chamber systems). Eddy flux measurements require high-resolution physico-chemical analysis procedures, which have been developed for only a few trace gases, such as water vapour, SO<sub>2</sub>, CO<sub>2</sub>, NO, NO<sub>2</sub>, and O<sub>3</sub> (e.g., Lenschow and Hicks, 1989). The technical requirements and the computer data management for these measuring techniques are considerable, but their results are representative for areas of several hectares extending upwind of the instruments (e.g., Delany et al.,

1986). Moreover, a prescription is required to interrelate the eddy fluxes well above the ground to those at the surfaces of vegetation and the soil, where the processes of deposition and emission take place.

On the contrary, measurements by enclosure techniques provide results of deposition or emission fluxes being representative only for small areas of up to a square metre (e.g., Slemr and Seiler, 1984). Representative results for larger areas can only be achieved with an array of chambers. Then, however, the technical requirements rapidly increase and may also exceed those for measuring eddy fluxes. Enclosure techniques are also inherently limited because they alter the local environment around the subject under study, in complete contrast to micrometeorological techniques (Baldocchi et al., 1988).

Since dry deposition tends to be extremely difficult to measure, the corresponding data set is still meager. Most flux estimates originate from individually conducted field experiments rather than from monitoring networks. To determine dry deposition by means of monitoring networks, mathematical models have to be used, which calculate the fluxes of atmospheric trace constituents on the basis of measured mean concentrations as well as mean meteorological quantities.

Currently, the inferential method seems to be the best available modelling tool to estimate dry deposition from monitoring data measured at a reference height  $z_R$  above ground. It is based on the flux-resistance analogy of the so-called constant flux theory for chemically conservative atmospheric trace gases expressed by (e.g., Wesely and Hicks, 1977)

$$F_i = -v_{d,i}c_{R,i} = \text{const.} \quad (1)$$

Here,  $F_i$  is the height-invariant vertical flux (density),  $v_{d,i} = (r_{t,i} + r_{mt,i} + r_{s,i})^{-1}$  is the deposition velocity, and  $c_{R,i} = c_i(z_R)$  is the mean concentration at the height  $z_R$ . Furthermore,  $r_{t,i}$  is the bulk resistance of the turbulent region of the atmospheric surface layer against mass transfer,  $r_{mt,i}$  is the corresponding bulk resistance of the underlying molecular-turbulent sublayer, and  $r_{s,i}$  is the bulk resistance of the canopy which characterizes the biochemical and physical processes taking place in the soil and within the plants.

Equation (1) was used, for instance, by Hicks et al. (1987) to infer dry deposition fluxes of  $\text{SO}_2$ ,

$\text{HNO}_3$ ,  $\text{O}_3$ , and particles on the basis of routine data on species concentrations, wind speed, standard deviation of the wind direction, temperature, humidity and global radiation.

Results from recent field experiments over agricultural crop fields and unmanaged grassland at different sites (e.g., Delany et al., 1986; Hicks and Matt, 1988) indicate that in the case of the highly reactive trace gases NO and  $\text{NO}_2$  (which are related to  $\text{O}_3$  by chemical reactions) the eddy fluxes directly measured and the mean concentrations concurrently determined disagree with the flux-resistance relationship expressed by Eq. (1). As pointed out by Delany et al. (1986) and Hicks and Matt (1988), some disagreement could be caused by emission of NO and  $\text{NO}_2$  from the soil. Results from model studies (e.g., Fitzjarrald and Lenschow, 1983; Kramm et al., 1991; Gao et al., 1991) also suggest that especially the fluxes of NO and  $\text{NO}_2$  can strongly vary with height because flux divergences can occur which are caused by chemical reactions between NO,  $\text{NO}_2$ , and  $\text{O}_3$ . Thus, some disagreement could also be attributed to these chemical reactions.

In view of these facts it is obvious that the use of the Eq. (1) to describe the exchange of NO and  $\text{NO}_2$  between the atmosphere and the biosphere could give false results, because  $r_{t,i}$  at least, is not definable for chemically reactive trace species. Moreover, the applicability of Eq. (1), especially in chemical transport models like RADM (Chang et al., 1987), where the turbulent resistance,  $r_{t,i}$ , is calculated for the lowest layer of the atmosphere of a thickness of several decameters, seems to be inadequate.

In our study, a SVAT scheme for estimating the exchange of NO,  $\text{NO}_2$ , and  $\text{O}_3$  is presented, where in contrast to Eq. (1), chemical reactions between these gases and NO emission are considered. This method is based on (a) an improved Deardorff-type SVAT scheme, which provides, among other things, the stomatal resistances for water vapour and trace gases using Jarvis's (1976) approach as well as the atmospheric fluxes of momentum, sensible and latent heat and the soil fluxes of sensible heat and moisture (Deardorff, 1978), and (b) the flux-resistance analogy for the canopy layer and the molecular-turbulent sublayer. The SVAT scheme has been tested on the basis of field data obtained over low vegetation (sugar beet) at Jülich/Germany in September 1984 (Höfken

et al., 1986). Sensitivity studies with different NO soil concentrations have been performed to demonstrate the effects of NO emission.

## 2. Model Description

### 2.1 The Flux-Resistance Relationship

#### 2.1.1 The Atmospheric Resistances

Analogous to the empirical mixing laws of micrometeorology, the flux  $F_i$  of a trace gas entity is written as (Sheppard, 1958)

$$F_i = -(D_i + K_i) \frac{\partial c_i}{\partial z}, \quad (2)$$

where  $D_i$  is the molecular diffusivity,  $K_i$  is the respective eddy diffusivity, and  $\partial c_i / \partial z$  is the vertical gradient of the (volumetric) concentration. Based on some empirical results that the turbulent transfers of sensible heat and water vapour are similar (e.g., Högström, 1967; Dyer and Hicks, 1970), which is adopted to the other scalars as well (e.g., Businger, 1986), it is assumed that  $K_i$  is equal to  $K_h$ , the eddy diffusivity of heat. This also agrees with empirical results derived from concurrent measurements of O<sub>3</sub> fluxes and O<sub>3</sub> profiles (Droppo, 1985).

Integrating Eq. (2) over the constant flux layer,  $z_s \leq z \leq z_R$ , provides (e.g., Herbert, 1987)

$$F_i = -r_{a,i}^{-1}(c_{R,i} - c_{s,i}) = \text{const.}, \quad (3)$$

where  $c_{s,i}$  is the concentration at the height of the receptor surface,  $z_s$ , and  $r_{a,i} = r_{t,i} + r_{mt,i}$  is the bulk resistance of the air against mass transfer. The resistances  $r_{t,i} = r_t$  and  $r_{mt,i}$  can be written as (e.g., Hicks, 1976)

$$r_t = \int_{\delta}^{z_R} K_h^{-1} dz = \frac{1}{u_* \kappa} \left( \ln \frac{z_R - d}{\delta - d} - \Psi_h(\zeta_R, \zeta_\delta) \right), \quad (4)$$

and (e.g., Owen and Thomson, 1963; Herbert, 1987)

$$r_{mt,i} = \int_{z_s}^{\delta} (D_i + K_h)^{-1} dz = (u_* B_i)^{-1}, \quad (5)$$

with (Schlichting, 1965; Kramm and Dlugi, 1994)

$$B_i^{-1} = \underbrace{Sc_i \int_0^{\eta_\delta} \frac{d\eta}{1 + Sc_i K_m / \nu}}_{I(Sc_i, \eta_\delta)} = \frac{c_{\delta,i} - c_{s,i}}{c_{*,i}}. \quad (6)$$

Here,  $u_*$  is the friction velocity,  $\kappa = 0.4$  is the von Kármán constant,  $\delta > d$  is the outer edge of the molecular-turbulent sublayer,  $d$  is the zero-plane displacement,  $\Psi_h(\zeta_R, \zeta_\delta)$  is the non-dimensional integral stability function for heat (Paulson, 1970; Kramm and Herbert, 1984),  $\zeta = (z - d)/L$  ( $L$  is the Monin-Obukhov stability length) is a non-dimensional height,  $K_m$  is the eddy diffusivity for momentum,  $\nu$  is the kinematic viscosity,  $Sc_i = \nu/D_i$  is the Schmidt number,  $\eta = u_* (z - z_s)/\nu$  is the roughness Reynolds number (or a non-dimensional height),  $\eta_\delta = u_* (\delta - z_s)/\nu$  is the non-dimensional thickness of the molecular-turbulent sublayer,  $c_{\delta,i}$  is the concentration at the height  $\delta$ , and  $c_{*,i}$  is the flux concentration related to the flux by  $F_i = -u_* c_{*,i}$ . The quantity  $B_i$  is the sublayer-Stanton number for the molecular-turbulent sublayer bordering the receptor surface. The quantities  $r_t$  and  $L$  are related to the turbulent height-invariant scaling parameters  $u_*$ ,  $\Theta_*$  (heat flux temperature) and  $q_*$  (water vapour flux concentration) which can similarly be determined on the basis of wind speed ( $U$ ), potential temperature ( $\Theta$ ), and specific humidity ( $q$ ) at the heights  $\delta$  and  $z_R$ .

As indicated by Eq. (6), the sublayer-Stanton number is a measure of the difference in the transfer rates of momentum and matter to and from rough (e.g., Owen and Thomson, 1963; Schlichting, 1965) and smooth surfaces (e.g., Brutsaert, 1975; Kramm et al., 1992), respectively. The causes of this difference are (a) momentum is destroyed at the surface by skin friction and form drag, and only the former has an analogy in mass and heat transfer, and (b) the molecular diffusion coefficient is not numerically equal to the analogous kinematic viscosity (Chamberlain, 1968). The quantity  $B_i$  can be considered to be a function of the roughness Reynolds number and the Schmidt number of the material being transferred.

There are several parameterization approaches for  $B_i$  derived from laboratory and field studies, which strongly differ from each other (e.g., Garratt and Hicks, 1973; Beljaars and Holtslag, 1991). These  $B_i$ -relationships are controversially discussed (Kramm et al., 1995) and require further consideration. However, to calculate the molecular-turbulent resistances  $r_{mt,fg,i}$  and  $r_{mt,i}$  (see Fig. 1), in this study (a) the modified Owen and Thomson relationship (Owen and Thomson, 1963)

$$B_i^{-1} = a Sc_i^b \eta_\delta^c, \quad (7)$$



water stress, temperature and carbon dioxide, respectively (see Appendix A).

The transfer through stomata is performed by molecular diffusion. Thus, in Eq. (11) the case of trace gases can be addressed by a simple correction factor  $g_{D,i} = D_i/D_0$ , where  $D_0$  refers to the molecular diffusivity at the initial values for  $r_{st,min}$  and  $b_{st}$  (usually that for water vapour), and  $D_i$  is the molecular diffusivity of the respective gas (e.g., Hicks et al., 1987).

In contrast to the stomatal resistance which can be estimated with sufficient accuracy, there exist only rough estimates for the resistances  $r_{int,i}^*$ ,  $r_{cu,i}^*$ ,  $r_{sl,i}^*$ ,  $r_{w,f,i}^*$  and  $r_{w,sl,i}^*$  (Wesely, 1989); but these quantities are assumed to be usually larger than the stomatal resistance, except for highly water-soluble trace gases like HNO<sub>3</sub> where the ‘effective’ resistances  $H_i \cdot r_{int,i}^*$ ,  $H_i \cdot r_{w,f,i}^*$  and  $H_i \cdot r_{w,sl,i}^*$  are much smaller.

In the case of low vegetation leaf resistances may be scaled according to the unit area of the ground surface (as a first approximation) by the amphistomatous leaf area index (LAI) (e.g., Hicks et al., 1987; Hanson and Lindberg, 1991). For taller vegetation and tree canopies with highly varying leaf area density (which leads to varying sorption conditions), it appears to be necessary to divide the canopy layer into several foliage layers, where for each foliage layer a resistance network analogous to that shown in Fig. 1 can be used, and where the exchange between the adjoining foliage layers can be described on the basis of a molecular-turbulent resistance similar to  $r_{mt,f,g,i}$  denoting the exchange between the lowest foliage layer and the ground.

As pointed out by Deardorff (1978), there is a rough relation between the shielding factor  $\sigma_f$  ( $0 \leq \sigma_f \leq 1$ ) associated with the degree to which the foliage prevents shortwave radiation from reaching the ground and the one-sided leaf area index given by  $LAI = 7 \sigma_f$ , which is consistent with results derived by Allan and Lemon (1972) for a corn crop and by Monteith et al. (1965) for barley. Assuming  $\sigma_f = 1$  and taking Eqs. (3), (9), and (10) as well as  $c_{s,i} = c_{f,i}$  into account, the flux,  $F_i (= F_{f,i})$  can be specified by (Kramm et al., 1991)

$$F_i = -v_{d,i}^* c_{R,i} = \text{const.} \quad (12)$$

with  $v_{d,i}^* = v_{d,i} (1 - \mu_i)$ , where  $v_{d,i}^*$  is denoted as an exchange velocity at the height  $z_R$  which is referred to the highest amount of the deposition veloc-

ity,  $v_{d,i}$  (given by Eq. (1)), by the expression  $1 - \mu_i$ . As shown in Kramm et al. (1991) as well as Kramm and Dlugi (1994), the quantities  $r_{s,i}$  and  $\mu_i$  in Eq. (12) can be derived from Eqs. (9) and (10).

## 2.2 Temperature and Moisture at the Surfaces of Foliage and Soil

The following flux budget equations for energy and moisture are used to calculate the temperature and the specific humidity at the surfaces of foliage and soil as required by the model:

### 2.2.1 Energy Budget of Foliage Surface

$$\begin{aligned} F_1((T_f, T_g, \eta_g)^T) = & R_{S,f} \downarrow - R_{S,f} \uparrow + R_{L,f} \downarrow \\ & - R_{L,f} \uparrow - (R_{S,g} \downarrow - R_{S,g} \uparrow) \\ & - (R_{L,g} \downarrow - R_{L,g} \uparrow) \\ & - (H_f + L_v(T_f) Q_f) = 0 \end{aligned} \quad (13)$$

### 2.2.2 Energy Budget of Soil Surface

$$\begin{aligned} F_2((T_f, T_g, \eta_g)^T) = & R_{S,g} \downarrow - R_{S,g} \uparrow + R_{L,g} \downarrow - R_{L,g} \uparrow \\ & - (H_g + L_v(T_g) Q_g) + H_s = 0 \end{aligned} \quad (14)$$

### 2.2.3 Water Budget of Soil Surface

$$F_3((T_f, T_g, \eta_g)^T) = W_s - Q_g = 0 \quad (15)$$

Here,  $R_S$  and  $R_L$  are the fluxes of shortwave and longwave radiation, where the values at the top of the canopy are denoted by subscript  $f$ , those at the ground by subscript  $g$ . The arrows  $\downarrow$  and  $\uparrow$  denote the direction of these fluxes. The quantities  $H$  and  $L_v(T) Q$  are the fluxes of sensible and latent heat within the atmosphere, where  $Q$  is the water vapour flux and  $L_v(T)$  is the temperature-dependent latent heat of vaporization,  $H_s$  and  $W_s$  are the total fluxes of heat and moisture within the soil,  $T_f$  and  $T_g$  are the surface temperatures of foliage and soil, and  $\eta_g$  is the volumetric moisture content at the soil surface, which is required to determine the corresponding specific humidity,  $q_g$ . In accord with Monteith (1975), Deardorff (1978), and Müller et al. (1993), the heat storage of the canopy has been neglected in our study. Furthermore, the specific humidity within the stomatal cavities was assumed to be saturated ( $q_i = q_i(T_f)$ ), even though experimental data indicate possible deviations from this “ideal” state (Ward and Bunce, 1986).

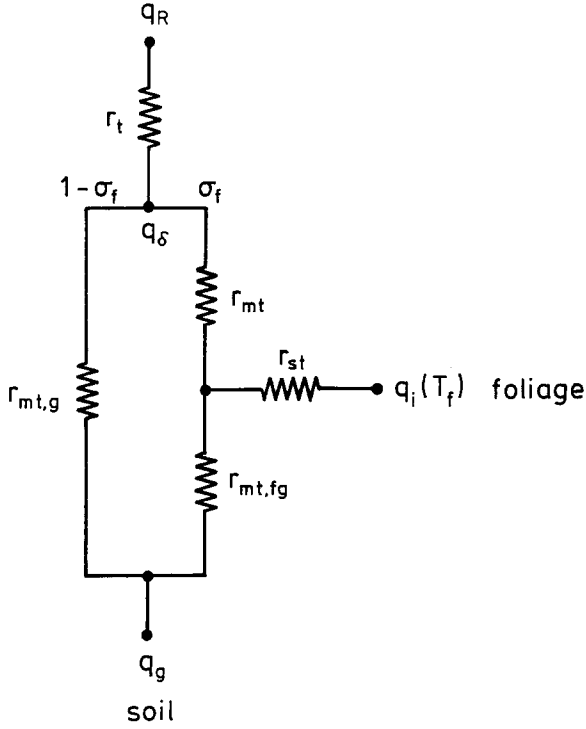


Fig. 2. Resistance network for describing the exchange of water vapour and sensible heat between the atmosphere and the vegetation-soil system. Note that in the case of heat exchange the specific humidity,  $q$ , has to be replaced by the potential temperature,  $\Theta$  (or the temperature  $T$ ), where the stomatal resistance,  $r_{st}$ , is not considered

The downward shortwave and longwave radiative fluxes  $R_{S,f}$  and  $R_{L,f}$  can be taken either from monitoring stations of a network or from simple parameterization schemes (e.g., Philipps, 1962) or more sophisticated radiative transfer models (e.g., Zdunkowski et al., 1982). The other radiative fluxes can be parameterized according to Dearsdorff (1978).

The heat and water vapour fluxes are given by (Kramm, 1995; see also Fig. 2)

$$H_f = -\sigma_f c_p \rho \left\{ \frac{1}{r_{mt,f}} (\Theta_\delta - T_f) + \frac{1}{r_{mt,fg}} (T_f - T_g) \right\} \quad (16)$$

$$Q_f = -\sigma_f \rho \left\{ \frac{1}{r_{mt,f}} (q_\delta - q_f) + \frac{1}{r_{mt,fg}} (q_f - q_g) \right\} \quad (17)$$

$$H_g = -c_p \rho \left\{ \frac{1-\sigma_f}{r_{mt,g}} (\Theta_\delta - T_g) + \frac{\sigma_f}{r_{mt,fg}} (T_f - T_g) \right\} \quad (18)$$

$$Q_g = -\rho \left\{ \frac{1-\sigma_f}{r_{mt,g}} (q_\delta - q_g) + \frac{\sigma_f}{r_{mt,fg}} (q_f - q_g) \right\}, \quad (19)$$

where  $\Theta_\delta$  and  $q_\delta$  are the values of potential temperature and specific humidity at the height  $\delta$ , and  $q_f$  is the specific humidity at the leaf surface. The quantities  $\Theta_\delta$ ,  $q_f$ , and  $q_\delta$  can be derived from Fig. 2 using Kirchhoff's laws of the electrostatics (see also Kramm, 1995).

## 2.2.4 The Soil Model

The soil model, which is used to calculate the fluxes of heat and water within the soil as required by Eqs. (14) and (15), is based on a set of two coupled partial differential equations for the soil temperature,  $T_s$ , and the volumetric moisture content,  $\eta$ , given by (Philip and de Vries, 1957; de Vries, 1958)

$$C \frac{\partial T_s}{\partial t} = -\frac{\partial H_s}{\partial z} \quad (20)$$

and

$$\rho_w \frac{\partial \eta}{\partial t} = -\frac{\partial W_s}{\partial z}, \quad (21)$$

where

$$H_s = -(\lambda + L_v \rho_w D_{T,v}) \frac{\partial T_s}{\partial z} - L_v \rho_w D_{\eta,v} \frac{\partial \eta}{\partial z} \quad (22)$$

and

$$W_s = -\rho_w \left( (D_{\eta,v} + D_{\eta,1}) \frac{\partial \eta}{\partial z} + D_{T,v} \frac{\partial T_s}{\partial z} + K_w \right) \quad (23)$$

represent the total fluxes of heat and moisture within the soil. Here,  $\rho_w$  is the density of liquid water,  $\lambda$  is the thermal conductivity,  $K_w$  is the hydraulic conductivity, and  $D_{T,v}$ ,  $D_{\eta,v}$  as well as  $D_{\eta,1}$  are the soil transfer coefficients. The volumetric heat capacity of the soil is defined by  $C = (1 - P) \rho_s c_s + \eta \rho_w c_w$ , where  $P$  is the porosity (which is equal to the maximum moisture content,  $\eta_s$ ),  $c_s$  is the specific heat capacity of the soil in a dry state,  $\rho_s$  is the soil density, and  $c_w$  is the specific heat capacity of water. Note that the heat capacity of air is negligible.

The thermal conductivity varies over several orders of magnitude as the soil dries out. It can be specified as a function of the soil moisture poten-

tial,  $\psi$ , by the empirical formula (McCumber and Pielke, 1981)

$$\lambda = \begin{cases} 419 \exp(-(Pf + 2.7)), & \text{if } Pf < 5.1 \\ 0.172, & \text{if } Pf > 5.1 \end{cases} \quad (24)$$

with  $Pf = {}^{10}\log \psi$ . The relationship between  $\psi$  and the relative humidity,  $h$ , can be expressed by (Edlefsen and Anderson, 1943)

$$h = \exp\left(\frac{g\psi}{R_d T_s}\right), \quad (25)$$

where  $R_d$  is the gas constant of water vapour.

The parameters  $\psi$  and  $K_w$  depend on the volumetric moisture content, the saturation hydraulic conductivity, and the porosity. This dependence can be expressed by (Clapp and Hornberger, 1978)

$$\psi = \psi_s \left(\frac{P}{\eta}\right)^b \quad (26)$$

and

$$K_w = K_{w,s} \left(\frac{\eta}{P}\right)^{2b+3}. \quad (27)$$

Taking these quantities into account, the soil transfer coefficients are given by (de Vries, 1958)

$$D_{T,v} = \alpha v_c D_v (P - \eta) \frac{\rho_d}{\rho_w} \frac{L_v(T_s) - g\psi}{R_d T_s^2} \quad (28)$$

$$D_{\eta,v} = -\alpha v_c D_v b \frac{P - \eta}{\eta} \frac{\rho_d}{\rho_w} \frac{g\psi}{R_d T_s} \quad (29)$$

$$D_{\eta,1} = -\frac{b K_{w,s} \psi_s}{\eta} \left(\frac{\eta}{P}\right)^{b+3}, \quad (30)$$

where  $D_v = 5.98 \cdot 10^{-8} T_s^{2.3}/p$  ( $p$  in hPa) is the molecular diffusivity for water vapour in air,  $\rho_d$  is the density of water vapour,  $\alpha$  is the torsion factor, and  $v_c = (1 - q_s)^{-1}$  is a correction factor. Since the specific humidity,  $q_s$ , within the soil is small,  $v_c$  may be approximated by  $v_c \approx 1$ .

As pointed out by Sasamori (1970), the total fluxes of heat and moisture can be considered as height-invariant within the uppermost soil layer having a thickness of a few millimetres. Integrating Eqs. (22) and (23) over this constant flux layer,  $z_{-1} \leq z \leq 0$ , provides the following approximations:

$$H_s \approx -\frac{1}{|z_{-1}|} ((\lambda + \rho_w L_v(T_m) D_{T,v}(T_m))(T_g - T_{-1}) + \rho_w L_v(T_m) D_{\eta,v}(\eta_m)(\eta_g - \eta_{-1})) = \text{const.} \quad (31)$$

$$\begin{aligned} W_s \approx & -\frac{\rho_w}{|z_{-1}|} (D_{\eta,v}(\eta_m)(\eta_g - \eta_{-1}) \\ & - \frac{b}{b+3} (\psi_g K_{w,g} - \psi_{-1} K_{w,-1}) \\ & + 0.5(K_{w,g} + K_{w,-1})|z_{-1}| \\ & + D_{T,v}(T_m)(T_g - T_{-1})) = \text{const.} \end{aligned} \quad (32)$$

Here,  $z_{-1}$  denotes the height of the uppermost grid level within the soil;  $T_{-1}$ ,  $\eta_{-1}$ ,  $\psi_{-1}$  and  $K_{w,-1}$  are the values of soil temperature, volumetric moisture content, soil moisture potential, and hydraulic conductivity at this level; and  $T_g$ ,  $\eta_g$ ,  $\psi_g$  and  $K_{w,g}$  are the corresponding values at the Earth's surface. The parameters  $L_v(T_m)$ ,  $D_{T,v}(T_m)$  and  $D_{\eta,v}(\eta_m)$  are functions of the mean quantities  $T_m = 0.5 (T_g + T_{-1})$  and  $\eta_m = 0.5 (\eta_g + \eta_{-1})$ .

The budget equations (13) to (15) reduce to a set of coupled non-linear equations which can be solved iteratively by a Newton-Raphson iteration procedure:

$$\mathbf{S}^{(n+1)} = \mathbf{S}^{(n)} - \mathbf{DF}(\mathbf{S}^{(n)})^{-1} \mathbf{F}(\mathbf{S}^{(n)}) \quad (33)$$

with

$$\mathbf{S} = \begin{Bmatrix} T_f \\ T_g \\ \eta_g \end{Bmatrix} \quad (34)$$

and

$$\mathbf{F}(\mathbf{S}) = \begin{Bmatrix} F_1(\mathbf{S}) \\ F_2(\mathbf{S}) \\ F_3(\mathbf{S}) \end{Bmatrix}. \quad (35)$$

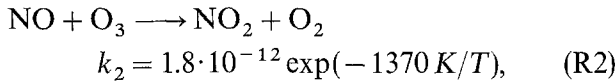
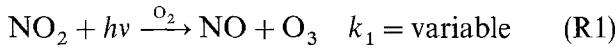
Here,  $\mathbf{DF}(\mathbf{S})$  is the functional matrix and  $\mathbf{DF}(\mathbf{S})^{-1}$  is the corresponding inverse matrix. The elements of  $\mathbf{DF}(\mathbf{S})$  may be calculated numerically (Kramm, 1995). The degree of accuracy for numerically solving the energy and moisture budget equations (i.e., Eqs. (13) to (15) and (33) to (35)) is determined by  $|F_1| < 0.1 \text{ W m}^{-2}$ ,  $|F_2| < 0.1 \text{ W m}^{-2}$ , and  $|F_3| < 10^{-7}$ , and is usually achieved after five to six iteration steps.

## 2.3 Kinetic Equations and Transfer Relations

### 2.3.1 The Reaction Scheme

Nitrogen dioxide predominantly occurs in the troposphere as a result of the oxidation of NO, which is mainly released in combustion processes. Its photodissociation by sunlight ( $\lambda < 430 \text{ nm}$ ,

e.g., Finlayson-Pitts and Pitts, 1986) leads to the formation of  $O_3$  via collision between an  $O(^3P)$  atom and an  $O_2$  molecule, where an  $N_2$  or  $O_2$  molecule usually serves as a third body. Ozone rapidly reacts with NO to regenerate  $NO_2$  so that in the absence of transfer processes and other chemical reactions a photostationary state between NO,  $NO_2$ , and  $O_3$  can be achieved. This simple reaction scheme can be summarized by (e.g., Finlayson-Pitts and Pitts, 1986)



where  $T$  is the air temperature in K. The photolysis frequency  $k_1$  is calculated as described by Kramm et al. (1991). The value of  $k_2$  (expressed in  $\text{cm}^3 \text{ molecule}^{-1} \text{ s}^{-1}$ ) is taken from Baulch et al. (1984).

The reaction scheme (R1) and (R2) ignores many chemical reactions involved in the photochemical smog formation. To consider a complex chemical mechanism for estimating dry deposition fluxes, the concentrations of about 20 to 25 trace gases would have to be known within the atmospheric surface layer. Such measurements have not been carried out so far. Therefore, our model calculations are restricted to the reactions (R1) and (R2). Even though the formation of  $HNO_3$  can also be addressed (Kramm et al., 1991), it is neglected here to illustrate the way in which our SVAT scheme can be used to estimate dry deposition or emission fluxes of NO,  $NO_2$ , and  $O_3$ .

### 2.3.2 Budget Equations and the Modified Profile Scheme

Assuming horizontal homogeneity where advection and horizontal flux divergence are neglected, the following set of coupled non-linear partial differential equations can be derived for the NO— $NO_2$ — $O_3$  triad (e.g., Lenschow, 1982)

$$\frac{\partial[NO_2]}{\partial t} = -\frac{\partial F_{NO_2}}{\partial z} - k_1[NO_2] + k_2[NO][O_3] \quad (36)$$

$$\frac{\partial[NO]}{\partial t} = -\frac{\partial F_{NO}}{\partial z} + k_1[NO_2] - k_2[NO][O_3] \quad (37)$$

$$\frac{\partial[O_3]}{\partial t} = -\frac{\partial F_{O_3}}{\partial z} + k_1[NO_2] - k_2[NO][O_3] \quad (38)$$

where  $[..]$  denotes the mean concentrations, and  $t$  the time. The reaction rate constant  $k_2$  in Eqs. (36) to (38) may be considered as  $k_2 = k_{0,2}(1 + I_s)$ , where  $k_{0,2}$  is the reaction rate constant experimentally derived within a reactor, and  $I_s = \langle \{NO\}' \{O_3\}' \rangle / ([NO][O_3])$  ( $-1 \leq I_s \leq 0$ ) is the intensity of segregation (e.g., Lenschow, 1982) which may play an important role in turbulent plumes of reacting species (e.g., Georgopoulos and Seinfeld 1986). The quantities  $\{NO\}'$  and  $\{O_3\}'$  are the fluctuating deviations from the respective mean concentrations, and  $\langle \dots \rangle$  represents the average. Obviously, the intensity of segregation would lead to a decrease of the 'true' reaction rate constant and, hence, to a decrease of the  $NO_2$  production rate (Vila-Guerau de Arellano and Duynkerke, 1993).

To estimate the influence of the intensity of segregation, it is useful to know whether the reaction (R2) is either kinetically limited ( $k_2 \approx k_{0,2}$ ) or diffusion limited ( $k_2 \leq k_{0,2}$ ). The Damköhler number,  $N_d$ , is a measure of the ratio of the characteristic diffusion time to the characteristic chemical reaction time for a given reaction. McRae et al. (1982) define those reactions with  $N_d > 50$  to be diffusion limited and those with  $N_d < 0.01$  to be kinetically limited. Introducing a turbulent Damköhler number for the reaction (R2) by (Stockwell, 1995)

$$N_{d,t} = \frac{k_{0,2}([NO] + [O_3])l^2}{2K_h}, \quad (39)$$

where  $l$  is the mixing length, provides a value of  $N_{d,t} < 0.08$  for neutral stratification and a reference height of  $z_R = 10$  m as well as moderate mean concentrations of  $O_3$  and NO. Hence, the reaction (R2) tends to be kinetically limited, and  $k_2$  is assumed to be  $K_{0,2}$ .

Equations (36) to (38) can be rearranged to provide the following budget equation system:

$$\frac{\partial c_j}{\partial t} = -\frac{\partial F_j}{\partial z} \quad (40)$$

with

$$c_j = \begin{cases} [NO_x] = [NO] + [NO_2] & \text{for } j = 1 \\ [O_x] = [NO_2] + [O_3] & \text{for } j = 2 \\ [NO_x] - [O_x] = [NO] - [O_3] & \text{for } j = 3 \end{cases} \quad (41)$$

and (with respect to Eq. (2)),

$$F_j = \begin{cases} -D_{\text{NO}_2} \frac{\partial[\text{NO}_2]}{\partial z} - D_{\text{NO}} \frac{\partial[\text{NO}]}{\partial z} - K_h \frac{\partial[\text{NO}_x]}{\partial z} & \text{for } j = 1 \\ -D_{\text{NO}_2} \frac{\partial[\text{NO}_2]}{\partial z} - D_{\text{O}_3} \frac{\partial[\text{O}_3]}{\partial z} - K_h \frac{\partial[\text{O}_x]}{\partial z} & \text{for } j = 2 \\ -D_{\text{NO}} \frac{\partial[\text{NO}]}{\partial z} + D_{\text{O}_3} \frac{\partial[\text{O}_3]}{\partial z} - K_h \frac{\partial([\text{NO}_x] - [\text{O}_x])}{\partial z} & \text{for } j = 3 \end{cases} \quad (42)$$

which no longer contains the chemical reactions (R1) to (R2) and, thus, describes the physical behaviour of chemically conservative trace gases. As shown in Eq. (40), the flux  $F_j$  of the ‘group’ concentration  $c_j$  will be independent of height if (quasi-) steady state conditions exist during the measurement interval. Thus, Eqs. (3) and (12) are assumed to be valid for estimating such height-invariant fluxes. This may be true for  $c_2$  because the Schmidt numbers and the Henry’s law constants of NO<sub>2</sub> and O<sub>3</sub> closely agree so that common values for  $r_{mt,i}$ ,  $r_{st,i}$ , and  $r_{int,i}$  could be considered in the case if both trace species are simultaneously deposited. However, the Schmidt number and the Henry’s law constant of NO differ from those of NO<sub>2</sub> and O<sub>3</sub>. Furthermore, emission and uptake of these nitrogen species can occur at the same site on separate occasions (e.g., emission of NO and deposition of NO<sub>2</sub>). Thus, it seems to be doubtful that the common use of any resistances depending on the characteristics of the ‘individual’ trace gases (which would lead to commonly used deposition and emission velocities) provides reasonable results. Moreover, environmental impact research requires a quantitative determination of the uptake of the ‘individual’ trace species, rather than that of the combinations mentioned above. Therefore, combined fluxes have to be separated to their ‘individual’ trace species and the chemical reactions among NO, NO<sub>2</sub>, and O<sub>3</sub> would have to be considered. Since, however, the relation between chemical transformation and transport processes within the canopy and the uptake or emission effects are highly complex, in the present study chemical reactions are considered only within the fully turbulent part of the atmospheric surface layer. Hence, a flux resistance relationship for the molecular-turbulent sublayer and the canopy layer given by (Kramm, 1991)

$$F_i = -\frac{c_{\delta,i}}{r_{mt,i} + r_{s,i}} (1 - \mu_i) = \text{const.} \quad (43)$$

is used. Here, the subscript  $i$  stands for NO, NO<sub>2</sub>, or O<sub>3</sub>.

The turbulent flux, for example, of O<sub>3</sub> can be calculated on the basis of a set of coupled non-linear ordinary differential equations, given by (Kramm, 1989)

$$\frac{\partial F_{\text{O}_3}}{\partial z} = k_1 c_2 - (k_1 + k_2 c_3)[\text{O}_3] - k_2 [\text{O}_3]^2 \quad (44)$$

$$\frac{\partial[\text{O}_3]}{\partial z} = -\frac{F_{\text{O}_3}}{K_h}. \quad (45)$$

This two-point boundary-value problem may numerically be solved with the shooting method and with reference to Gear’s (1971) backward differentiation formulae.

Routine data of wind speed, temperature, humidity and concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> serve as upper boundary conditions at the height  $z_R$ . The lower boundary conditions, i.e., the concentrations of the ‘individual’ trace species at the height  $\delta$  and the ‘group’ concentrations  $c_1$ ,  $c_2$ , and  $c_3$  at the same height have to be calculated simultaneously. Here, the calculations of the lower boundary conditions are based on the requirement that the flux divergences  $\partial F_{\text{NO}}/\partial z$ ,  $\partial F_{\text{NO}_2}/\partial z$ , and  $\partial F_{\text{O}_3}/\partial z$  vanish at the height  $\delta$  so that the right side of Eq. (44) can be considered as equal to zero. This leads to the chemical equilibrium between NO, NO<sub>2</sub>, and O<sub>3</sub>. The requirement is a consequence of the constant flux approximation expressed in Eq. (43) on which the resistance approach for the molecular-turbulent sublayer and the canopy layer is based even in the case of chemically reactive trace species. This approximation agrees with that used in enclosure techniques for determining the canopy and molecular-turbulent resistances. The calculation of the lower

boundary conditions can only be carried out iteratively (see Kramm and Dlugi, 1994; Kramm, 1995). When the lower boundary conditions have been determined, equation set (44) and (45) can be solved. The 'group' concentrations  $c_1$ ,  $c_2$ , and  $c_3$  can be calculated along with the eddy diffusivity  $K_h$  for each level  $\delta \leq z \leq z_R$ .

### 3. Model Tests and Preliminary Results

Data of wind speed, temperature, humidity and concentrations averaged over a certain period are employed to numerically determine the vertical fluxes of momentum, sensible and latent heat, NO, NO<sub>2</sub>, and O<sub>3</sub>. Unfortunately, at present only a few data sets of these mean quantities exist which allow testing of our SVAT scheme. Moreover, the evaluation of our model on the basis of the trace gas fluxes and the corresponding fluxes of momentum, sensible and latent heat simultaneously measured during the SANA field campaign SADE '94 by eddy correlation techniques at two heights (Beier et al., 1995) has to be postponed until the results of these flux measurements are available.

Vertical fluxes of momentum, sensible and latent heat as well as NO, NO<sub>2</sub>, and O<sub>3</sub> were

determined on the basis of wind speed, dry-bulb temperature, specific humidity, and the concentrations of these trace gases measured by the Institute of Atmospheric Chemistry III at the Forschungszentrum (KFA) Jülich at heights of 0.40, 2.60 and 17.20 m above an even terrain, covered with sugar beet (25 cm tall), near Jülich in western Germany in September 1984 (Höfken et al., 1986). Wind speed and temperature data were averaged over 5 min. Concentrations of NO and NO<sub>2</sub> (2 min averages) were determined by chemiluminescent techniques applying a modified commercial NO/NO<sub>2</sub>/NO<sub>x</sub> analyser (Thermo Electron 14A) with a detection limit of 0.1 ppb. An UV absorption method (Dasibi 1003-AH, 1 ppb detection limit) was used to measure the O<sub>3</sub> concentration (2 min averages). These data were also used by Kramm (1989) and Kramm et al. (1991) to compute the vertical profiles of wind speed, temperature, humidity and concentrations and the corresponding turbulent fluxes (see Figs. 3 and 4). In contrast to those calculations, in the present study only the data observed at the 17.2 m level are used. Neither soil temperature and soil moisture nor compensation point concentrations were measured under field conditions. Moreover, the determination of  $\sigma_f$  and the plant-specific

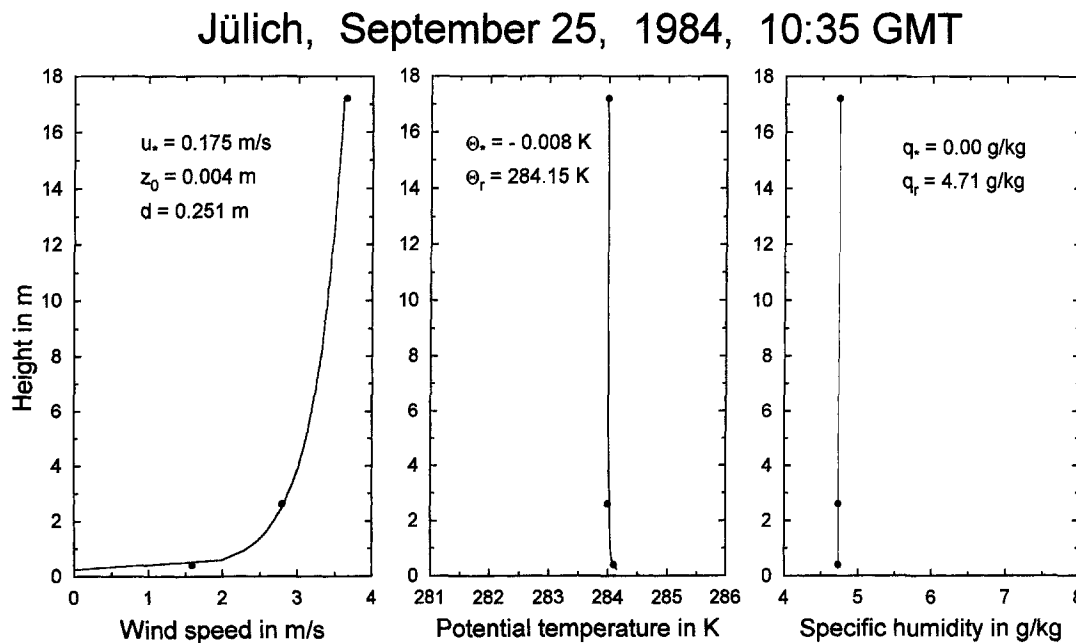


Fig. 3. Vertical profiles of wind speed, potential temperature and specific humidity. The solid symbols represent the measured values (Höfken et al., 1986), and the lines the calculated vertical profiles (Kramm et al., 1991)

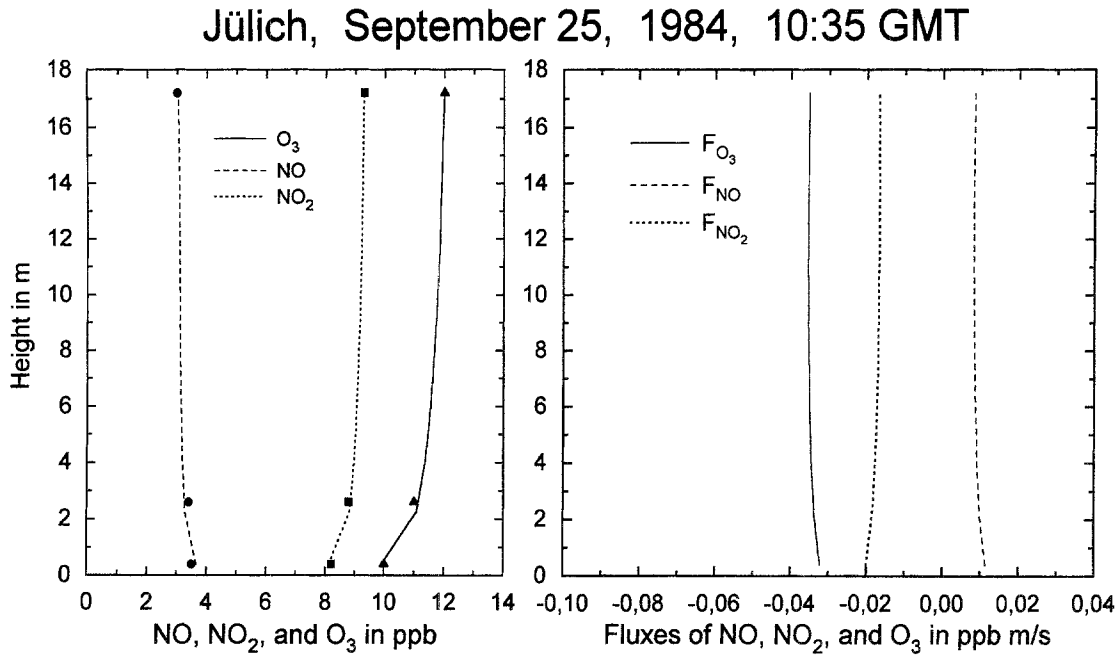


Fig. 4. As in Fig. 3, but for concentrations and turbulent fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub>

Table 1. *Input Data used for Model Tests*

| Atmosphere:                                                                                          |                                 |                   |                   |                     |                          |                         |
|------------------------------------------------------------------------------------------------------|---------------------------------|-------------------|-------------------|---------------------|--------------------------|-------------------------|
| $z$<br>(m)                                                                                           | $U$<br>(m/s)                    | $\Theta$<br>(K)   | $q$<br>(g/kg)     | NO<br>(ppb)         | NO <sub>2</sub><br>(ppb) | O <sub>3</sub><br>(ppb) |
| 17.2                                                                                                 | 3.65                            | 283.99            | 4.73              | 3.0                 | 9.3                      | 12.0                    |
| $R_{s,f}\downarrow = 165 \text{ W/m}^2$ (estimated), $z_0 = 0.004 \text{ m}$ , $d = 0.251 \text{ m}$ |                                 |                   |                   |                     |                          |                         |
| Soil (arbitrarily chosen):                                                                           |                                 |                   |                   |                     |                          |                         |
| $z_{-1}$<br>(m)                                                                                      | $T_{-1}$<br>(K)                 | $\eta_{-1}$       | $P$               | $K_{w,s}$<br>(m/s)  | $\psi_s$<br>(m)          | $b$                     |
| -0.025                                                                                               | 281.0                           | 0.2               | 0.435             | $3.4 \cdot 10^{-5}$ | -0.218                   | 4.9                     |
| Vegetation (arbitrarily chosen):                                                                     |                                 |                   |                   |                     |                          |                         |
| $r_{st,min}$<br>(s/m)                                                                                | $b_{st}$<br>(W/m <sup>2</sup> ) | $T_{min}$<br>(°C) | $T_{max}$<br>(°C) | $T_{opt}$<br>(°C)   |                          |                         |
| 65                                                                                                   | 10                              | 5                 | 45                | 25                  |                          |                         |

parameters as required in Jarvis's formulae (see Eq. (11) and Appendix A) could not be carried out, and adequate values were not found in the literature. Therefore, the values of soil temperature and soil moisture as well as plant-specific quantities were chosen arbitrarily. The input data used in our study are listed in Table 1.

Figure 5 shows results for the vertical profiles of wind speed, temperature and humidity provided by the SVAT scheme. These results were derived for different values of  $\sigma_f$  ranging from  $\sigma_f = 1$  (i.e., the soil is totally covered by vegetation) to  $\sigma_f = 1/7$  (i.e., nearly bare soil). They indicate that the thermal stratification varies from slightly unstable to stable when  $\sigma_f$  decreases. Figure 6 shows the influence of  $\sigma_f$  upon the sensible and latent heat fluxes above the vegetation and between the foliage and the soil as well as the soil heat flux.

Compared with the results shown in Fig. 3, only the results derived for a soil surface totally covered by vegetation ( $\sigma_f = 1$ ) seem to be adequate for the input values that were arbitrarily chosen (Table 1). Therefore, only the results of the vertical fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> derived for  $\sigma_f = 1$  are discussed.

The results illustrated in Fig. 4 suggest that in the case of the Jülich data the turbulent fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> are nearly height-invariant. Since the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> at the heights of 0.4 m, 2.6 m and 17.2 together with the NO<sub>2</sub> photolysis frequency,  $k_1 = 0.087 \text{ min}^{-1}$  (cloud cover = 8/8), and the reaction rate constant  $k_2 = 22.1 \text{ ppm}^{-1} \text{ min}^{-1}$  indicate a photostationary state characterized by the Leighton relationship, the calculation of the turbulent fluxes of these trace species has to provide height-invariant

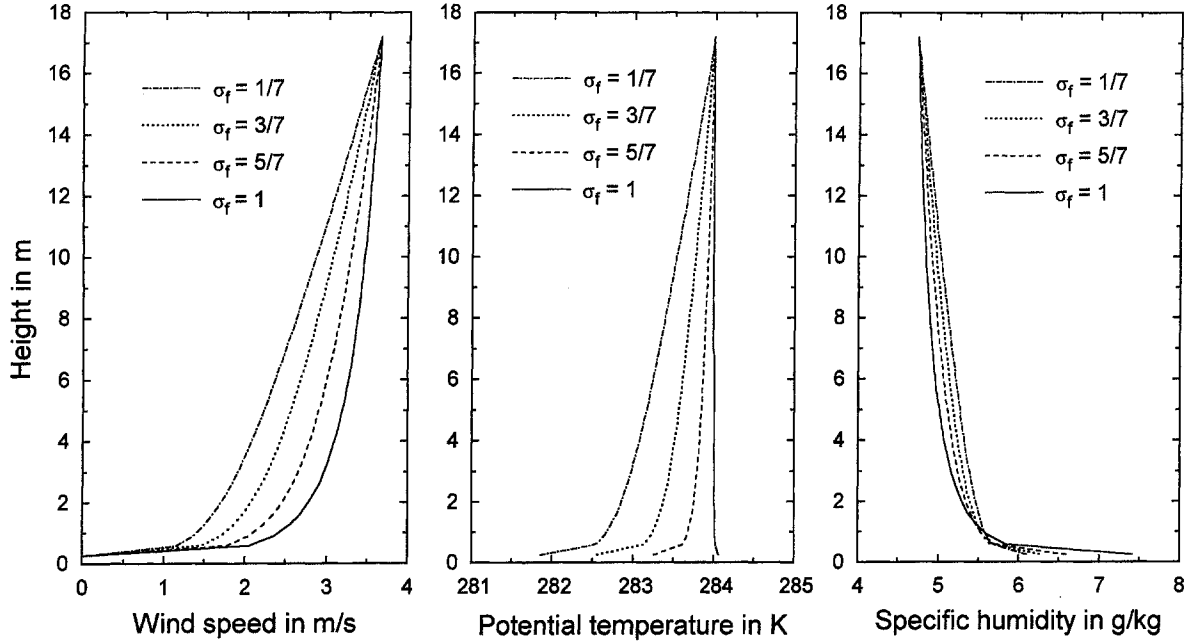


Fig. 5. Vertical profiles of wind speed, potential temperature and specific humidity calculated for different values of the shielding factor,  $\sigma_f$

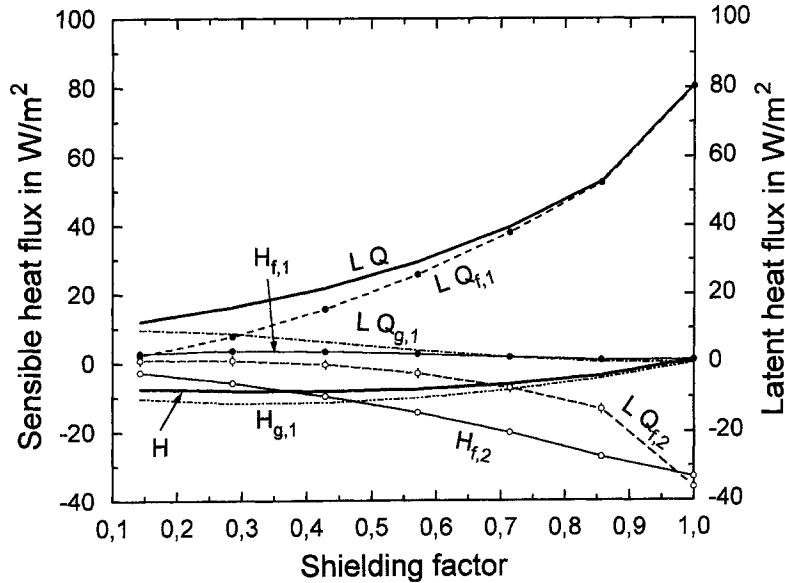


Fig. 6. Plot of the fluxes of sensible and latent heat vs. shielding factor,  $\sigma_f$ . Here,  $H$  and  $LQ$  are the turbulent fluxes above vegetation,  $H_{f,1}$  and  $LQ_{f,1}$  are the fluxes between the foliage and the height  $\delta$ ,  $H_{g,1}$  and  $LQ_{g,1}$  are the fluxes between the bare soil surface and the same height, and  $H_{f,2}$  and  $LQ_{f,2}$  are the fluxes between the foliage and the soil surface

fluxes, even if chemical reactions are included. Although the influence of chemical reactions on dry deposition (or emission) fluxes of  $\text{NO}$ ,  $\text{NO}_2$ , and  $\text{O}_3$  cannot be well demonstrated on the basis of these data, we have, nevertheless, used these data due to the lack of better data at present.

Test results of sensitivity studies regarding deposition and emission of  $\text{NO}$  and  $\text{NO}_2$  are illustrated in Figs. 7 and 9. Arbitrary values of  $c_{\text{sl},\text{NO}}$

ranging from zero to 35 ppb, and  $c_{\text{sl},\text{NO}_2}$  ranging from zero to 12 ppb, were used to switch from deposition to emission or vice versa (see also Table 3), where substrate concentrations of  $\text{O}_3$  were neglected. The sensitivity studies were performed for a nearly dry foliage surface. Typical results of the calculated values of the molecular-turbulent resistances and the substrate resistances are listed in Table 2.

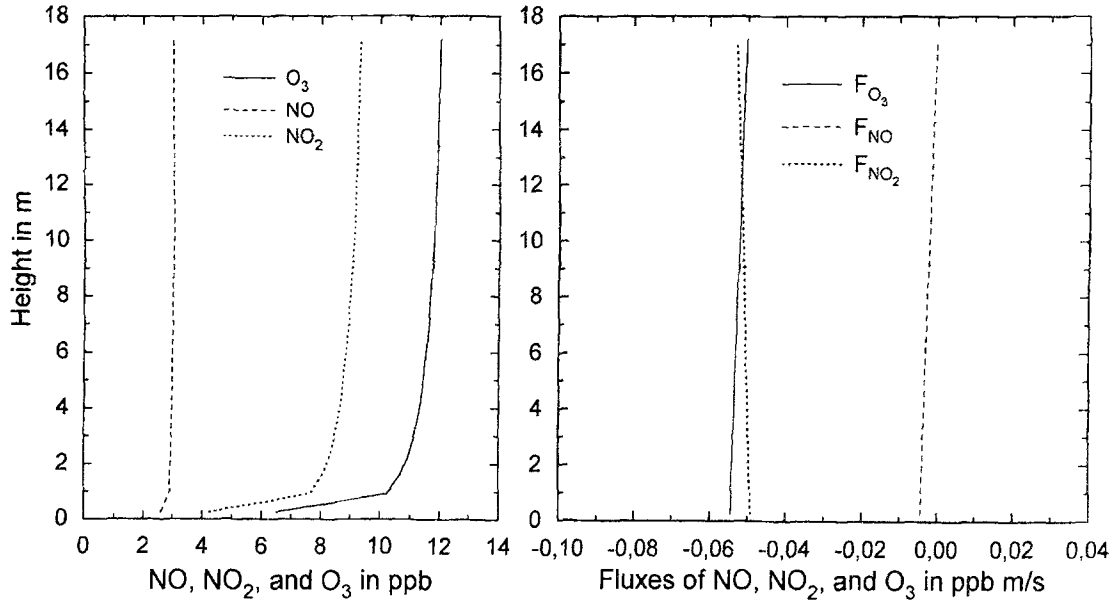


Fig. 7. Vertical profiles of concentrations and turbulent fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> for  $c_{sl,NO} = c_{sl,NO_2} = 0$

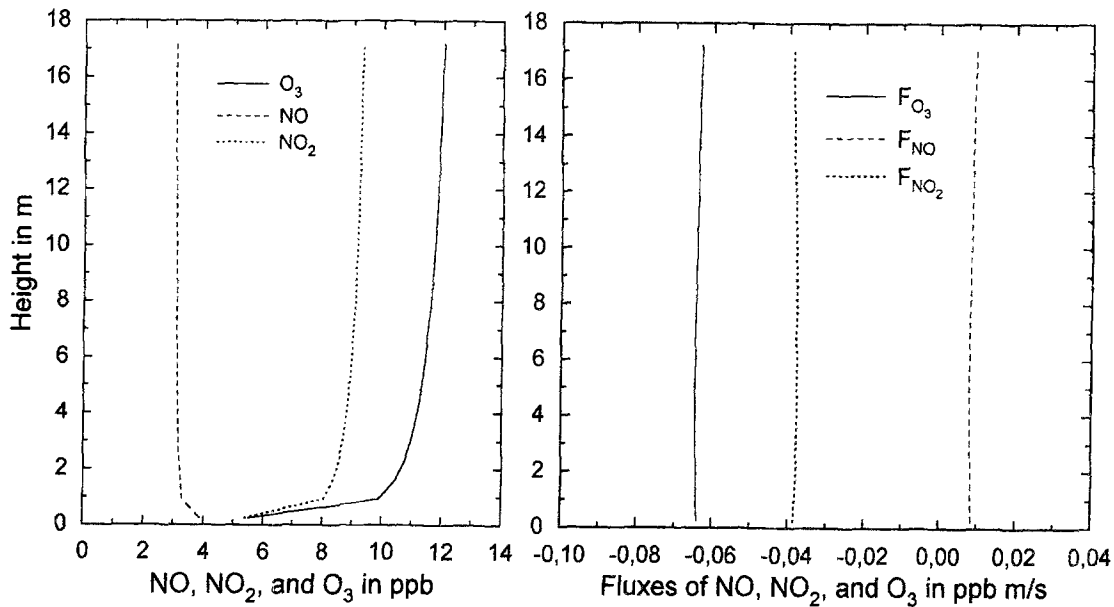


Fig. 8. As in Fig. 7, but for  $c_{sl,NO} = 22$  ppb,  $c_{sl,NO_2} = 12$  ppb

Figure 7 illustrates that in the case of  $c_{sl,NO} = c_{sl,NO_2} = 0$  (maximum deposition) the fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> considerably differ from those shown in Fig. 4. The same is true in the case of increasing  $c_{sl,NO}$  values ( $c_{sl,NO_2} = 0$ ). The shapes of the vertical flux profiles are similar for all states, where especially the deposition fluxes of NO and NO<sub>2</sub> decrease. The vertical concentration profiles are nearly identical except close to

the ground, where the profile values show small differences. The compensation point concentration of NO amounts to about 9 ppb. Similar results can be obtained for increasing  $c_{sl,NO_2}$  values ( $c_{sl,NO} = 0$ ), but in this case a compensation point concentration could not be determined.

Since the results of these sensitivity studies did not agree with those of Fig. 4, further attempts with different soil concentrations of NO and NO<sub>2</sub>

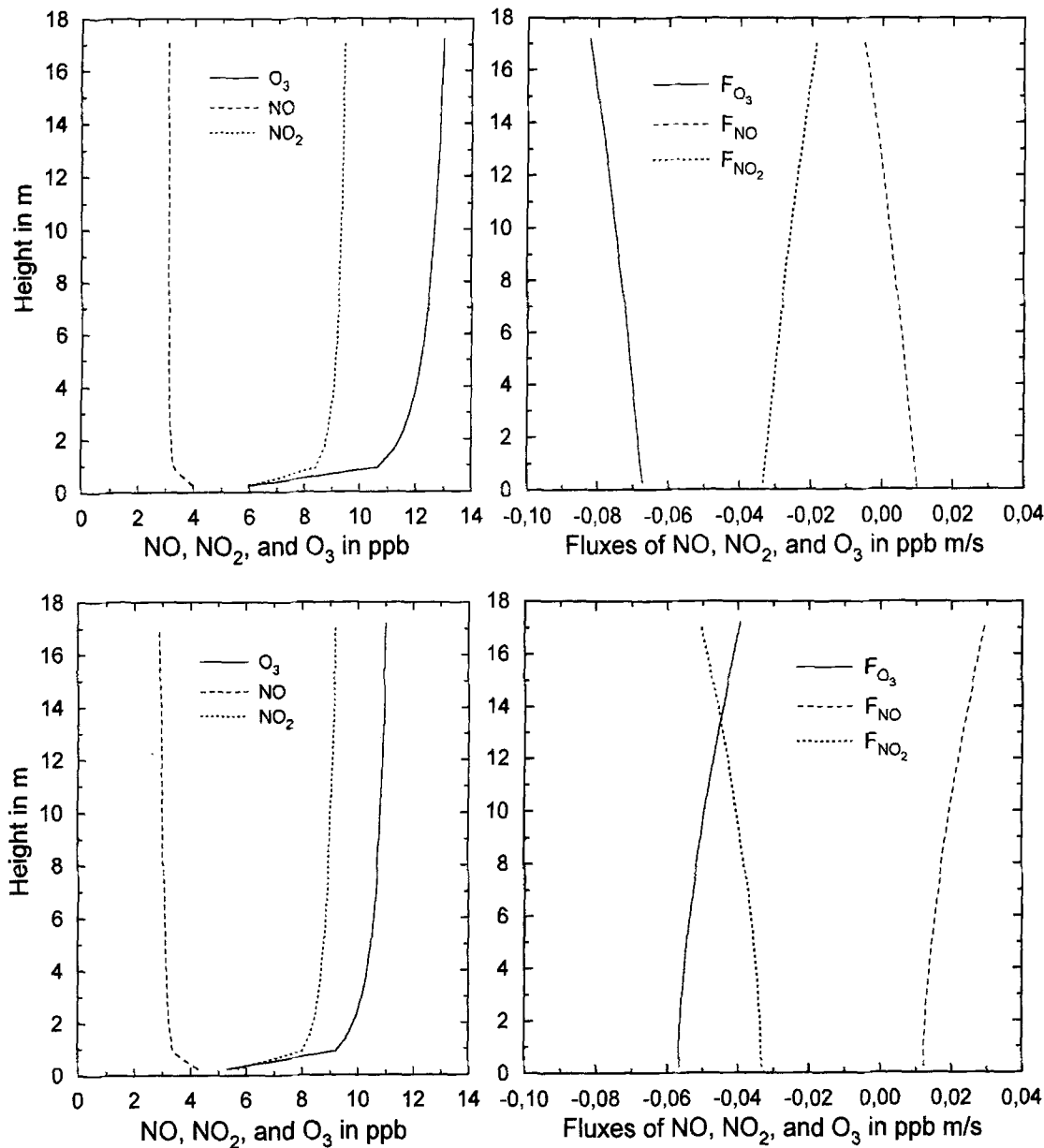


Fig. 9. As in Fig. 8, but for concentrations arbitrarily altered by  $\pm 100$  ppt (NO and NO<sub>2</sub>) and  $\pm 1$  ppb (O<sub>3</sub>)

both greater than zero were made to achieve a better agreement. In comparison with the results shown in Fig. 4 the “best” agreement was obtained for  $c_{\text{sl,NO}} = 22$  ppb and  $c_{\text{sl,NO}_2} = 12$  ppb (see Fig. 8), where, however, the deposition fluxes of NO<sub>2</sub> and O<sub>3</sub> are more than 50% larger as indicated in Fig. 4. Seemingly, a better agreement can be achieved if measurements of soil-specific concentrations (dependent on soil temperature and soil moisture) and plant-specific parameters are available. Therefore, these quantities should concurrently be determined with the eddy fluxes

of trace gases, momentum, sensible and latent heat as well as the vertical profiles of concentrations, wind speed, temperature and humidity in future field experiments designed for model evaluation.

Usually, the incoming solar radiation or the photolysis frequency of NO<sub>2</sub>,  $k_1$ , can be measured with a sufficient degree of accuracy. Furthermore, the value of the reaction rate constant  $k_2$  is widely accepted so that the accuracy of the calculated flux profiles may be sufficient (discrepancies in the results when the  $k_2$  value is changed were already

Table 2. *Calculated Resistances for NO, NO<sub>2</sub>, and O<sub>3</sub>. Note that the Values of  $r_{st,i} = 500 \text{ s m}^{-1}$  and  $r_{w,i} = 500 \text{ s m}^{-1}$  were Arbitrarily Chosen. Furthermore, the Value  $\mu_{\text{NO}}$  corresponds to a Substrate Concentration of  $c_{sl,\text{NO}} = 5 \text{ ppb}$*

|                                         | NO     | NO <sub>2</sub> | O <sub>3</sub> |
|-----------------------------------------|--------|-----------------|----------------|
| Resistances is $\text{s m}^{-1}$ -Units |        |                 |                |
| $r_{st,i}^{\alpha}$                     | 167.5  | 206.1           | 206.1          |
| $H_i \cdot r_{int,i}^{\beta}$           | 9400.0 | 500.0           | 500.0          |
| $r_{cu,i}$                              | 2152.5 | 2649.5          | 2649.5         |
| $r_{s,i}$                               | 178.0  | 72.7            | 72.7           |
| $r_{mt,i}$                              | 27.2   | 31.2            | 31.2           |
| $r_{mt,fg,i}^{\gamma}$                  | 82.1   | 96.9            | 96.9           |
| $\mu_i$                                 | 0.63   | 0.0             | 0.0            |
| $H_i$                                   | 22.6   | 4.3             | 4.6            |
| $Sc_i$                                  | 0.72   | 0.88            | 0.88           |

<sup>$\alpha$</sup>  According to Jarvis (1976), Eqs. (11) of the present study.

<sup>$\beta$</sup>  Values of NO and NO<sub>2</sub> taken from O'Dell et al. (1977), the O<sub>3</sub> value corresponds to that of NO<sub>2</sub>.

<sup>$\gamma$</sup>  According to Eq. (7) of our study.

discussed by Kramm et al., 1991). However, uncertainties in the flux profiles may also be affected by a small displacement in the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub>. Such a displacement can be substantiated by the detection limits of chemical sensors.

To investigate this aspect in the vicinity of a photostationary state as considered here, the concentration values of NO and NO<sub>2</sub> were arbitrarily altered by 100 ppt and the concentration value of O<sub>3</sub> by 1 ppb. Results derived for the soil concentrations  $c_{sl,\text{NO}} = 22 \text{ ppb}$  and  $c_{sl,\text{NO}_2} = 12 \text{ ppb}$  are illustrated in Fig. 9. As expected, these results indicate that in the vicinity of the photostationary state a small displacement in the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> can produce large discrepancies in the flux results, which are manifested here by the shift from height-invariant fluxes substantiated by the photostationary state to strongly height-dependent fluxes realized by the departure from that state. Since the alteration of the O<sub>3</sub> concentration mainly contributes to these discrepancies in the flux results, the accuracy with which this concentration can be measured has to be improved to derive reliable flux estimates.

To calculate the lower boundary conditions at the outer edge of the molecular-turbulent sublayer,

Table 3. *Results of the Ozone Fluxes,  $F_{\text{O}_3,mt}$  and  $F_{\text{O}_3,t}$ , calculated for the Lower Boundary  $\delta$*

| Case                              | $c_{sl,\text{NO}}$<br>(ppb) | $c_{sl,\text{NO}_2}$<br>(ppb) | $F_{\text{O}_3,mt}$<br>(ppb m/s) | $F_{\text{O}_3,t}$<br>(ppb m/s) |
|-----------------------------------|-----------------------------|-------------------------------|----------------------------------|---------------------------------|
| 1                                 | 0                           | 0                             | −0.063                           | −0.055                          |
| 2                                 | 5                           | 0                             | −0.060                           | −0.057                          |
| 3                                 | 9                           | 0                             | −0.058                           | −0.059                          |
| 4                                 | 12                          | 0                             | −0.057                           | −0.060                          |
| 5                                 | 0                           | 5                             | −0.064                           | −0.054                          |
| 6                                 | 0                           | 9                             | −0.064                           | −0.053                          |
| 7                                 | 12                          | 12                            | −0.059                           | −0.058                          |
| 8                                 | 22                          | 12                            | −0.055                           | −0.062                          |
| 9 <sup><math>\alpha</math></sup>  | 0                           | 0                             | −0.060                           | −0.048                          |
| 10 <sup><math>\alpha</math></sup> | 22                          | 12                            | −0.052                           | −0.056                          |

<sup>$\alpha$</sup>  Upper boundary conditions were altered (see text).

the requirement that the flux divergences  $\partial F_{\text{NO}}/\partial z$ ,  $\partial F_{\text{NO}_2}/\partial z$ , and  $\partial F_{\text{O}_3}/\partial z$  vanish at the height  $\delta$  was introduced which leads to the chemical equilibrium between NO, NO<sub>2</sub>, and O<sub>3</sub>. This requirement is a consequence of the constant flux approximation expressed in Eq. (43) on which the resistance approach for the molecular-turbulent sublayer and the canopy layer is based. Although the theoretical concept is formulated in a consistent manner, there are still some problems in matching the fluxes at the height  $\delta$  (see also Kramm and Dlugi, 1994). Typical flux results obtained by the flux-resistance relationship for the molecular-turbulent sublayer and the canopy layer,  $F_{\text{O}_3,mt}$ , and those derived for the turbulent region using the shooting method,  $F_{\text{O}_3,t}$  are listed in Table 3. This table indicates differences between these two fluxes as large as 20%. It seems that these differences are produced by the small amounts of the eddy diffusivity at the outer edge of the molecular turbulent sublayer. Since the flux-resistance relationship and the eddy diffusivity are used to derive the start values for the shooting method, the small amount of the eddy diffusivity can produce large discrepancies between the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> and the corresponding calculated concentrations at the upper boundary  $z_R$ . Thus, the shooting

method requires a new iteration step and, hence, the flux amount calculated for the lower boundary,  $\delta$ , differs from that derived by the flux-resistance relationship (43). Therefore, the requirement mentioned above as well as the matching of the fluxes demand further investigations. This includes, of course, the parameterization of the transfer of matter and heat across the molecular-turbulent sublayer when highly reactive trace gases are considered.

#### 4. Summary and Conclusions

A SVAT scheme for determining the dry deposition and/or emission fluxes of NO, NO<sub>2</sub>, and O<sub>3</sub> in the atmospheric surface layer over horizontally uniform terrain covered with fibrous canopy elements was presented and discussed. Its preliminary results suggest that these dry deposition fluxes are not only influenced by meteorological and plant-physiological parameters, but also by chemical reactions among these trace species as well as NO emission from the soil. A small displacement in the concentrations of NO, NO<sub>2</sub>, and O<sub>3</sub> within the range of the detection limits of the chemical sensors, for instance, can produce large discrepancies in the flux estimates which are manifested here by the shift from height-invariant to strongly height-dependent fluxes. Consequently, (a) the relatively large detection limit of O<sub>3</sub> analysers has to be reduced to derive reliable flux estimates, and (b) the widely used 'big leaf' multiple resistance approach, which is based on the constant flux approximation, seems to be inappropriate for computing dry deposition fluxes and deposition velocities of NO and NO<sub>2</sub>.

Obviously, final evaluation of the model presented here must be postponed until the fluxes of these species directly measured together with those of momentum, sensible and latent heat during the SADE '94 campaign by eddy correlation techniques at two heights (Beier et al., 1995) are finally evaluated.

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#### Appendix A

Following Jarvis (1976) and Hicks et al. (1987), the correction functions can be expressed by

$$g_{\delta}(\delta_e) = 1 - b_e \delta_e, \quad (A1)$$

$$g_{\psi}(\psi) = \begin{cases} 1, & \text{if } \psi > \psi_t \\ a_{\psi}\psi + b_{\psi}, & \text{if } \psi \leq \psi_t \end{cases} \quad (A2)$$

$$g_T(T_f) = \frac{T_f - T_{\min}}{T_{\text{opt}} - T_{\min}} \left[ \frac{T_{\max} - T_f}{T_{\max} - T_{\text{opt}}} \right]^{b_T} \quad (A3)$$

with

$$b_T = \frac{T_{\max} - T_{\text{opt}}}{T_{\text{opt}} - T_{\min}}, \quad (A4)$$

and

$$g_c(\text{CO}_2) = \begin{cases} 1, & \text{if } [\text{CO}_2] \leq 100 \\ 1 - b_{c1}[\text{CO}_2], & \text{if } 100 < [\text{CO}_2] < 1000 \\ b_{c2}, & \text{if } [\text{CO}_2] > 1000. \end{cases} \quad (A5)$$

Here,  $\delta_e = e_s(T) - e$  is the water vapour deficit (where  $e_s(T)$  is the saturated water vapour pressure at air temperature  $T$ , and  $e$  is the ambient water vapour pressure),  $\psi$  is the leaf water potential,  $\psi_t$  is a species-dependent threshold value,  $T_f$  is the temperature of the foliage,  $[\text{CO}_2]$  is the ambient CO<sub>2</sub> concentration in ppmv,  $T_{\min}$  and  $T_{\max}$  are species-dependent higher and lower temperature extremes at which stomata no longer open, respectively. The quantity  $T_{\text{opt}}$  is the temperature at which stomatal exchange is optimized. The quantities  $b_e$ ,  $a_{\psi}$ ,  $b_{\psi}$ ,  $b_{c1}$ , and  $b_{c2}$  are empirical constants dependent on the plant species. Values for  $r_{\text{st},\min}$ ,  $b_{\text{st}}$ ,  $T_{\min}$ , and  $T_{\text{opt}}$ , for instance, are given by Jarvis (1976), Körner et al. (1979), Hicks et al. (1987), and Baldocchi et al. (1987). Note that  $g_c(\text{CO}_2) = 1$  was arbitrarily chosen for our model studies.

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